

Induction hardening: Effect of Bainite in the Case Layer on Fatigue Strength

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Acknowledgments

This project was financed by the Swedish Heat Treatment Centre – a collaborative research centre hosted by Swerea for applied research on heat treatment in close cooperation with Swedish manufacturing industry.

Objective

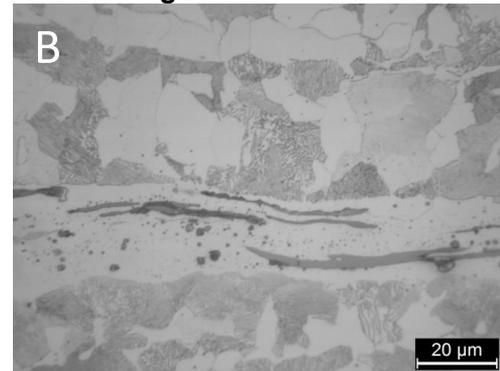
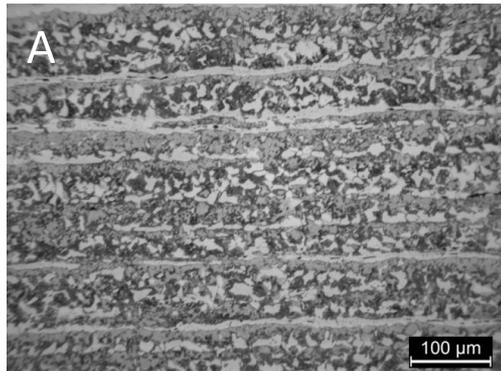
- To investigate how bainite content in the case layer affects fatigue strength of induction hardened components.
- To provoke bainite formation in the case layer by altering the induction hardening process.

Material: Steel grade C45 (AISI 1045)

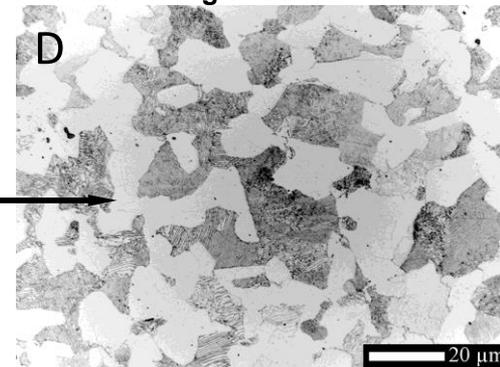
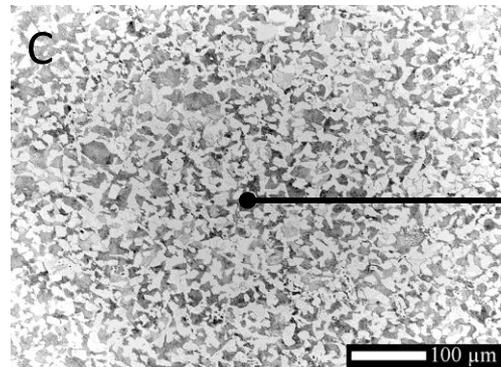
Alloying content of C45 (AISI 1045)

C	Si	Mn	P	S	Cr	Ni	Mo	Cu
0.44	0.20	0.68	0.014	0.030	0.15	0.15	0.03	0.23

Microstructure as delivered in rolling direction



Microstructure as delivered in cross-rolling direction



Methods: Provoke bainite formation

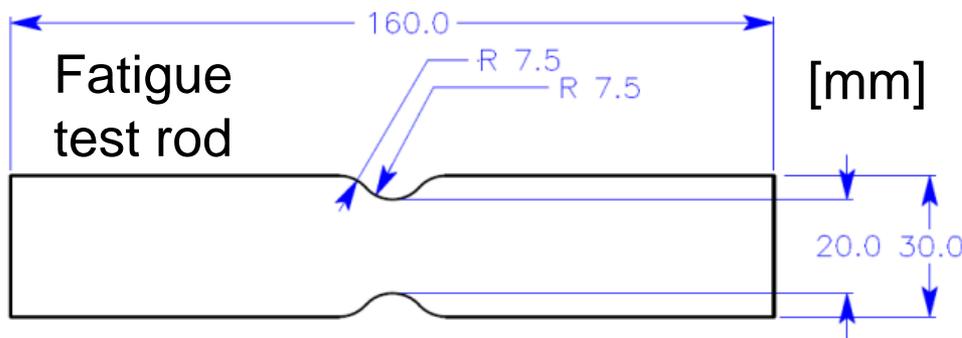
To provoke bainite formation a number of concepts were discussed:

- I. Pre-heating to reach a higher core temperature.
- II. Quench delay after heat treatment to change temperature gradient.
- III. Reduce quenching power by flow or polymer concentration.
- IV. Final surface temperature by changing heating power.
- V. Affect hardenability by changing steel heat or grade.
- VI. Partly dissolved as-delivered microstructure after heating.
- VII. Turning after heat treatment to achieve a bainitic surface zone.

Methods: Induction hardening

Induction heating:

- Frequency: 22 kHz
- Rotation: 300 rpm
- Power: 70 kW
- Heating time: 4.3 s
- Peak temperature: 985C



Induction hardening of test rods



Methods: Quenching

Stahl Ck45
(Schmelze 3)

Zeit-Temperatur-Umwandlungs-Schaubild
(kontinuierlich)

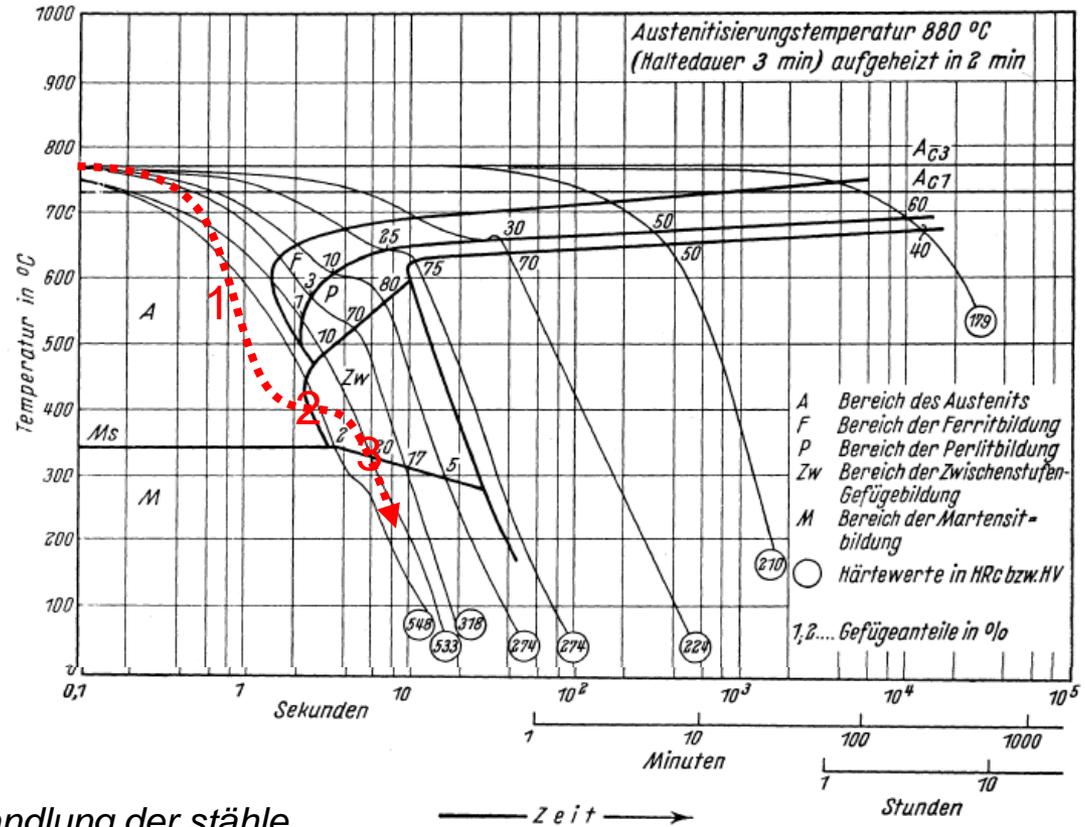
II-101 E

Chemische Zusammensetzung	C	Si	Mn	P	S	Cr	Cu	Mo	Ni	V
	0,44	0,22	0,66	0,022	0,029	0,15	—	—	—	0,02

C45 has low hardenability.

Quenching:

1. Fast to avoid formation of ferrite and pearlite.
2. Short interrupt at the bainite regime.
3. Fast to form martensite



Reference: CCT from Atlas zur wärmebehandlung der stähle

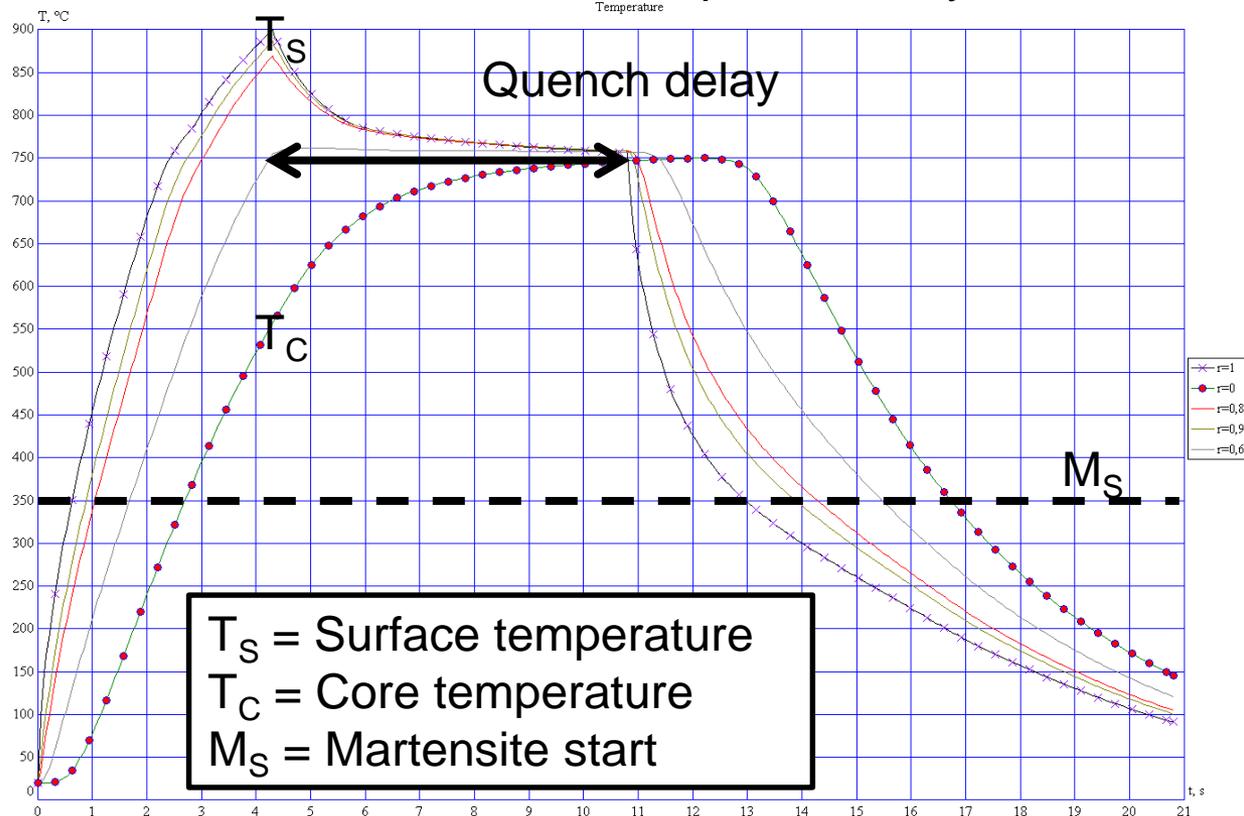
Methods: Quenching

- A screening study was done to evaluate induction hardening with quench delay and interrupted quenching. Based on the findings three series of fatigue test bars were produced:

Series	Description (as programmed in PLC)
A – Reference	Direct quenching for 30 seconds.
B – Quench delay	2.5 s holding time before 30 seconds quenching.
C – Interrupted quench	Quenching for 0.6 seconds, then 0.8 seconds quench interruption followed by 30 seconds final quenching.

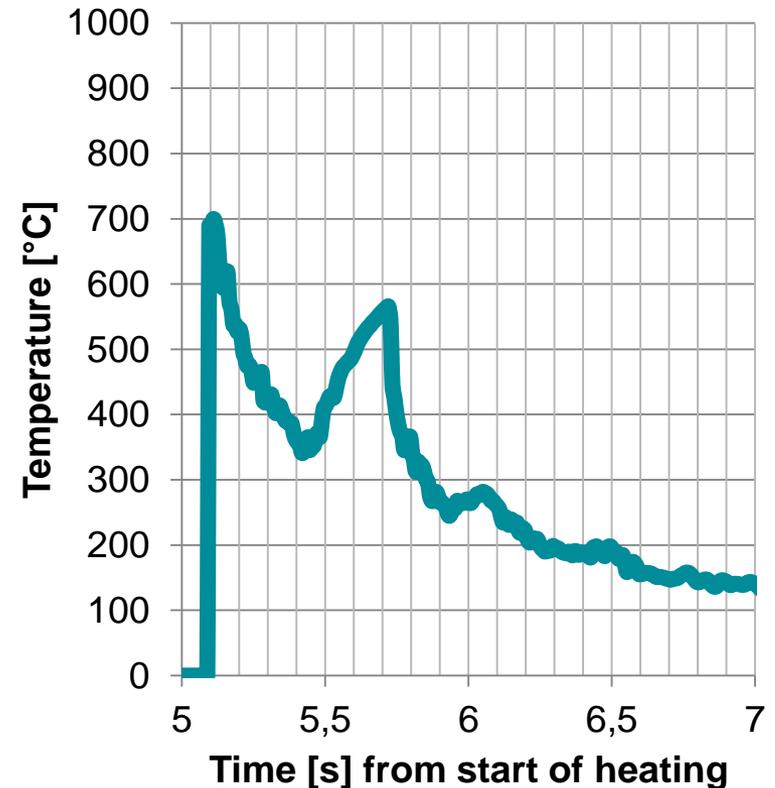
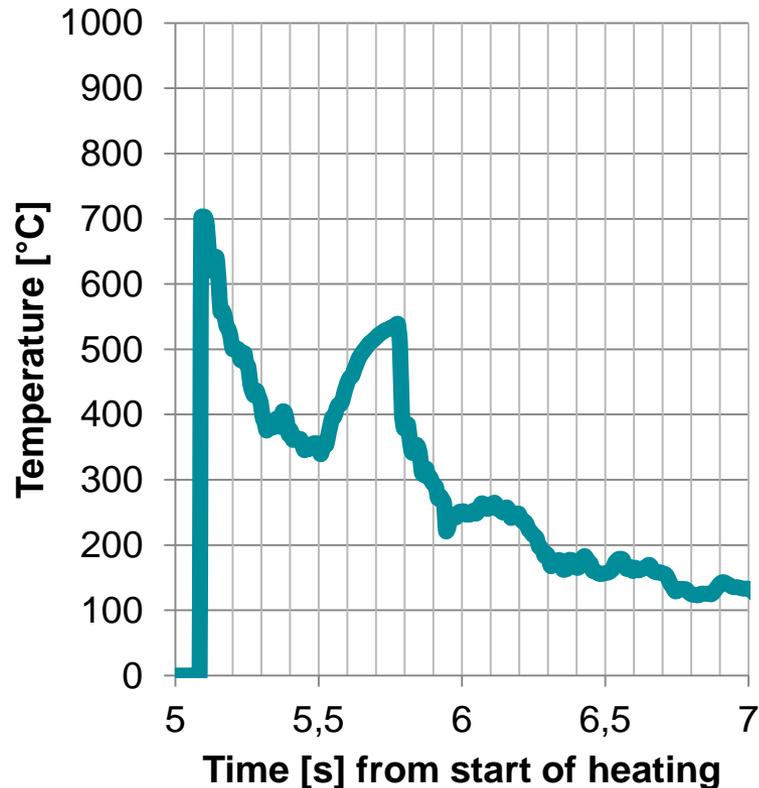
Methods: Quenching

ELTA simulation of quench delay.

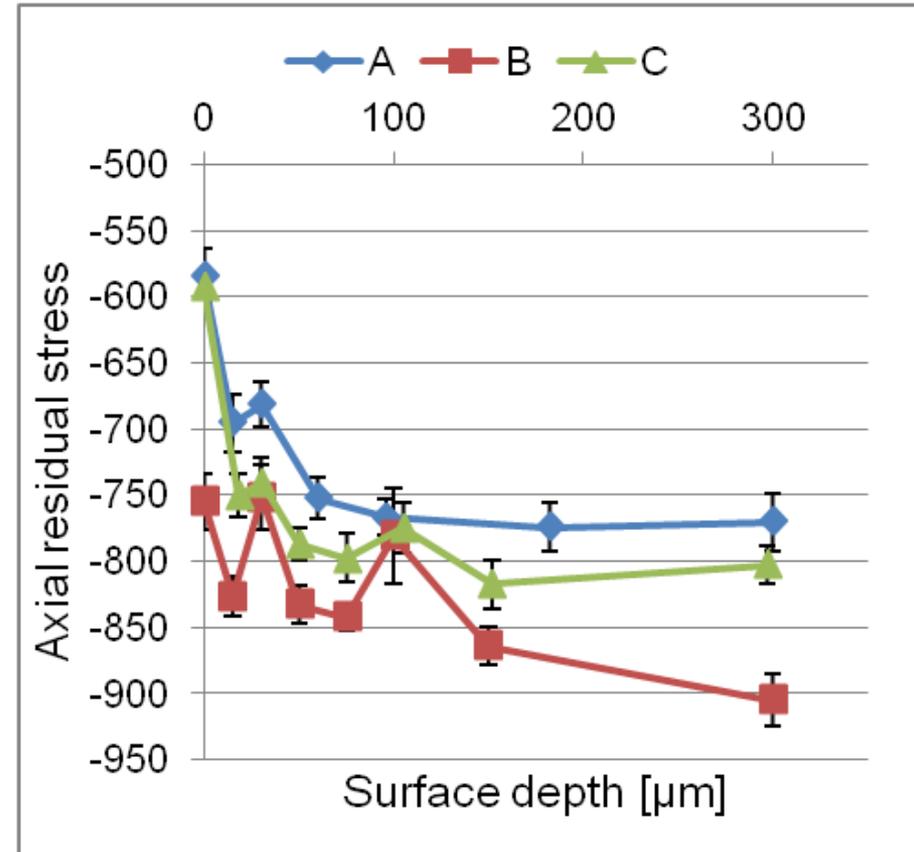
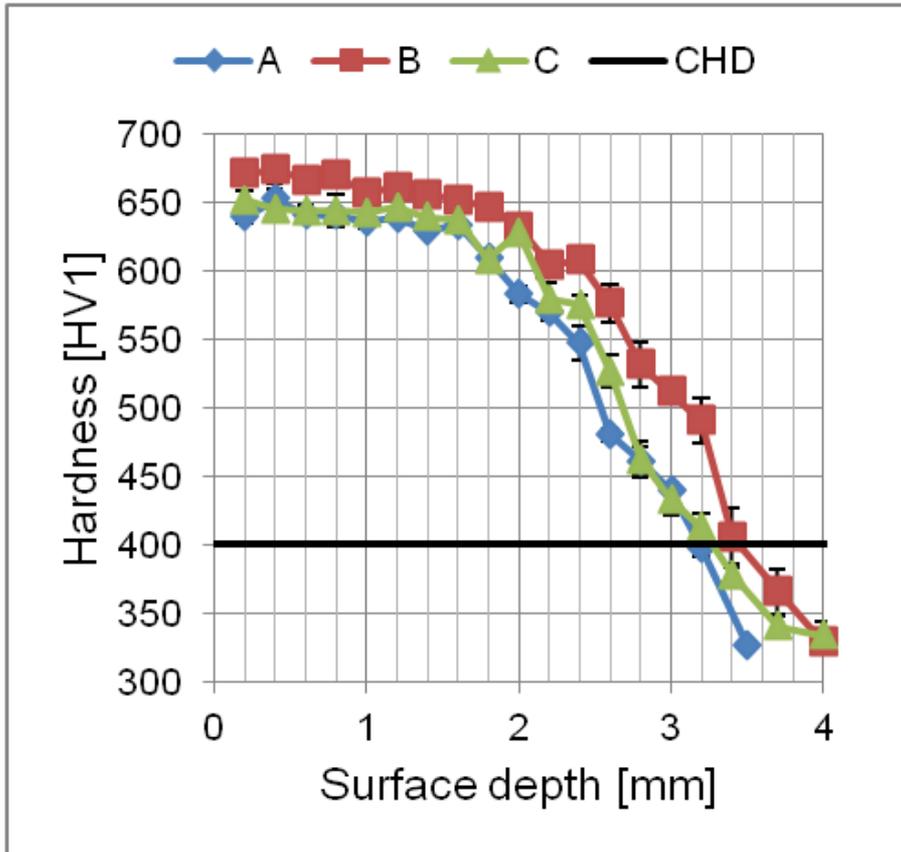


Methods: Quenching

Interrupted quench, Series C, temperature measurements showed good repeatability. Temperature profiles show data from two heat treatments.



Results: Hardness and Residual stresses

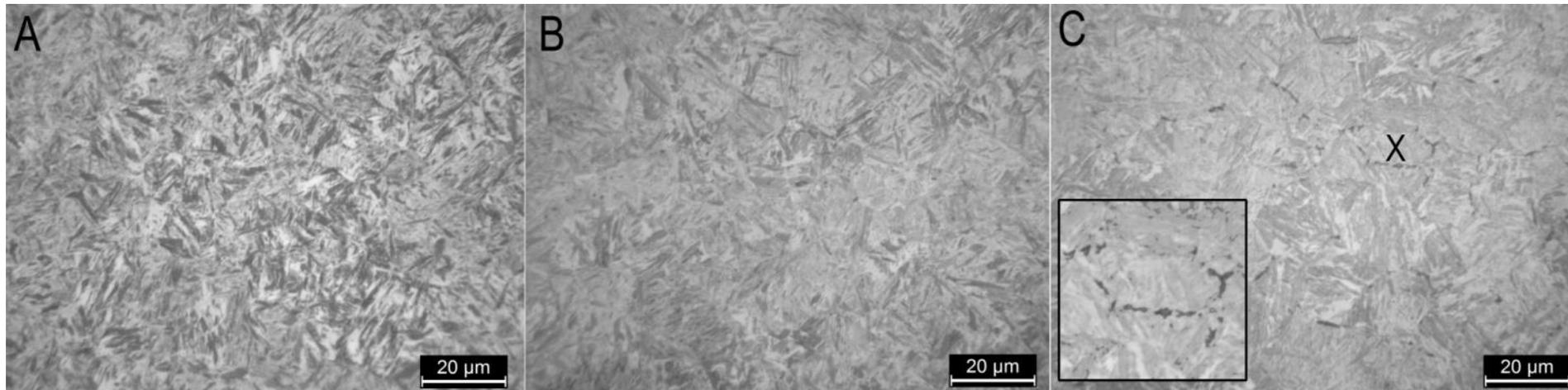


Results: Microstructure characterization

To define the presence of bainite we adopted:

“ B_T “: Depth with first tendency for bainite formation in 1000x magn.

“ B_U “: Depth with apparent bainite formation in 200x magn.



A – Reference

B_T : 1.0 mm depth

B_U : 1.4 mm depth

B – Quench delay

B_T : 0.8 mm depth

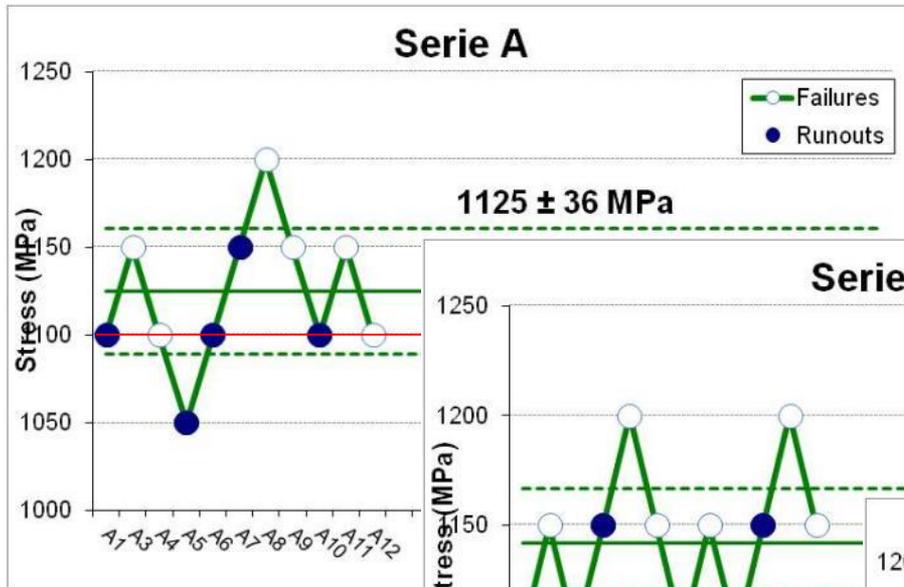
B_U : 1.4 mm depth

C – Interrupted quench

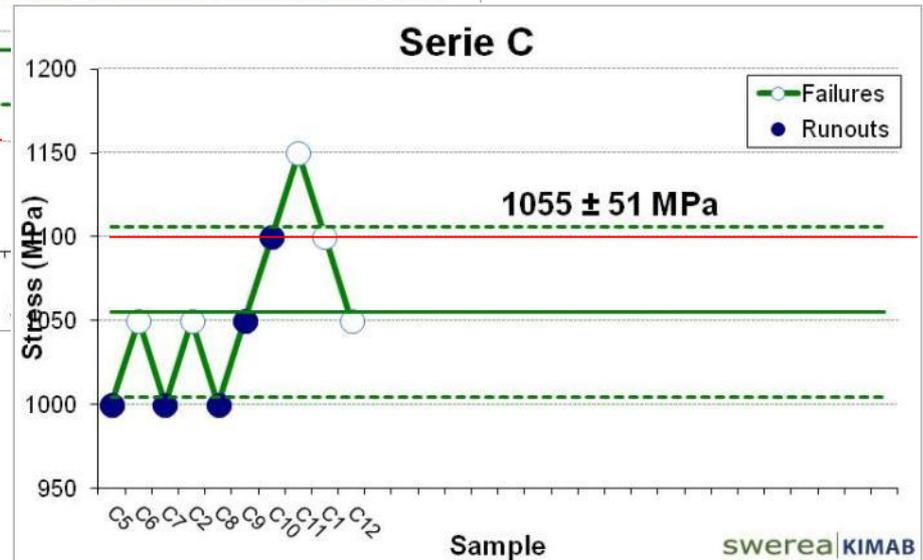
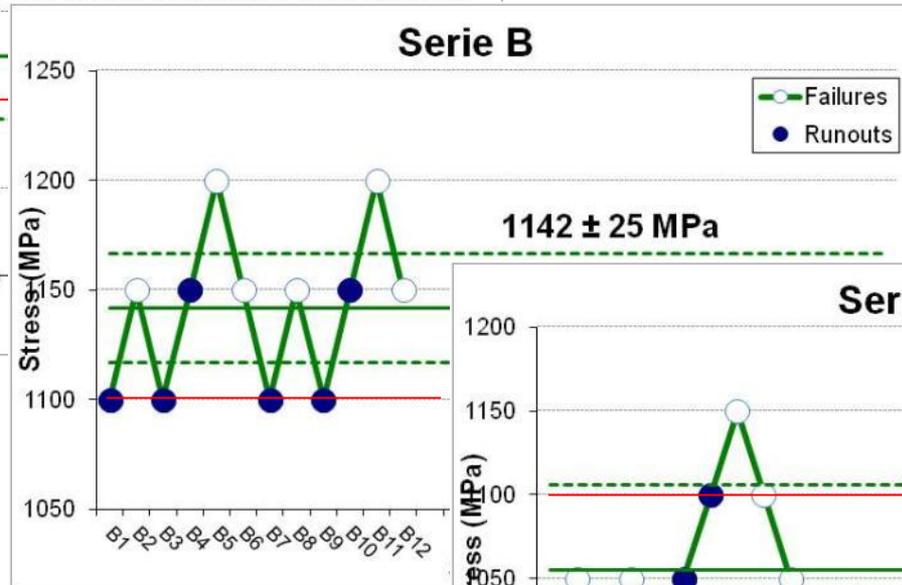
B_T : 0.1 mm depth

B_U : 0.4 mm depth

Results: Fatigue testing



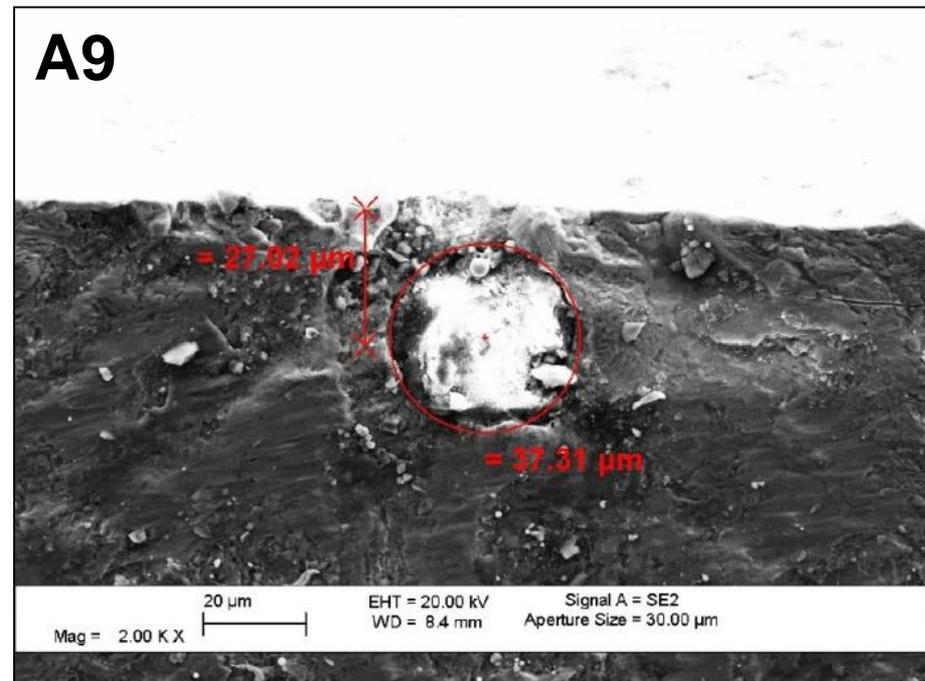
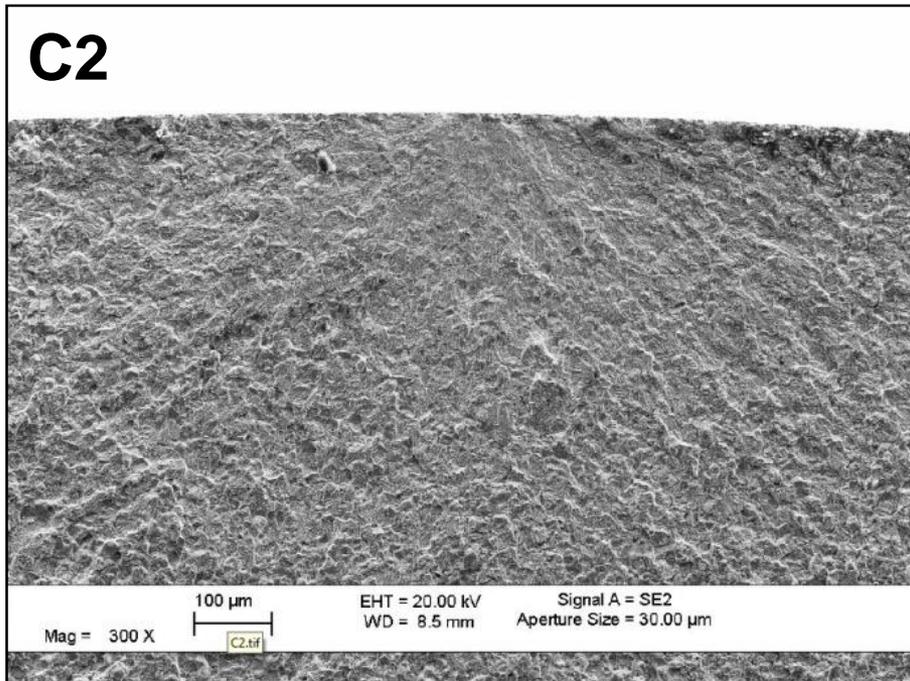
The 1100 MPa level has been marked by a red line in all figures.



Series C, with bainite in the case layer, shows a 75 MPa lower fatigue strength, when compared to series A och B.

Results: Fractography

Fractography micrographs showed surface initiation: (left) fracture surface of test rod C2, which is representative for all failed fatigue test rods except A9. (right) fracture surface of test rod A9 where a relative large inclusion was observed.



Results: Summary

Results from characterization of fatigue test rods.

	SHD	CHD	RSt	RSa	B_T	B_U	FS
Series A	640HV	3.2 mm	710	695	1.0 mm	1.4 mm	1125 ± 36 MPa
Series B	670HV	3.4 mm	920	825	0.8 mm	1.4 mm	1142 ± 25 MPa
Series C	650HV	3.2 mm	760	750	0.1 mm	0.4 mm	1055 ± 51 MPa

Details of fatigue testing – runouts and failures.

	Series A		Series B		Series C	
Stress level [MPa]	Runout	Failure	Runout	Failure	Runout	Failure
1000	-	-	-	-	3	-
1050	1	-	-	-	1	3
1100	3	2	4	-	1	1
1150	1	3	2	4	-	1
1200	-	1	-	2	-	-
Total	5	6	6	6	5	5

Conclusion

- In summary, the results from the present work suggest that bainite will have a negative impact on fatigue strength of induction hardened steel-components. However, small amounts of bainite will neither affect hardness nor residual stresses; hence impact on fatigue strength by bainite is most likely facilitation of crack initiation and -growth.



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