# e2V

## e2v technologies

The data to be read in conjunction with the Hydrogen Thyratron Preamble.

### **ABRIDGED DATA**

Hollow anode, deuterium-filled two-gap thyratrons with metal/ceramic envelope, featuring high peak current, high rate of rise of current, low jitter and >50% voltage/current reversal. They have been developed specifically for use in low inductance circuits associated with excimer lasers.

The patented hollow anode structure enables the tube to cope with inverse voltage and current without consequent reduction in its high voltage hold off capability due to electrode damage.

A reservoir normally operated from a separate heater supply is incorporated. The reservoir heater voltage can be adjusted to a value consistent with anode voltage hold-off in order to achieve the fastest rate of rise of current possible from the tube in the circuit

The CX1725W is structurally identical to the CX1725, which is rated for peak forward voltage of 70 kV max, peak forward current of 15 kA max and average current of 5 A. These ratings are not simultaneous. The internal deuterium gas pressure of the CX1725W is optimised at the factory for efficient operation at the following conditions:

Peak forward anode voltage	. 31	kV max
Peak forward anode current	5	kA max
Peak reverse anode current	2	kA max
Average anode current	2.0	A max
Rate of rise of current	>300	kA/μs
Jitter	1.0	ns
Pulse repetition rate	. 400	pps max

### **GENERAL DATA**

#### **Electrical**

Cathode barium aluminate impregnated tungste	en
Cathode heater voltage (see note 1) 6.3 $\pm$ 0.3	V
Cathode heater current	Α
Reservoir heater voltage (see note 1) $6.3 + 0.7 - 0.3$	V
Reservoir heater current 7.0	Α
Tube heating time (minimum) 10.0 m	in

#### Mechanical

Seated height			240 mm (9.449 inches) max
Clearance required below	/		
mounting flange			. 80 mm (3.150 inches) min
Overall diameter (excludi	ng		
connections)			122 mm (4.803 inches) max
Net weight			. 3.6 kg (8 pounds) approx
Mounting position			see note 2
Tube connections			see outline

## CX1725W Liquid Cooled, Hollow Anode Two-Gap Metal/Ceramic Thyratron



### Cooling

The tube must be cooled by total liquid immersion, for example in force-circulated transformer oil (see e2v technologies Technical Reprint No. 108 'The cooling of oil-filled electrical equipment, with special reference to high power line-type pulse generators' by G. Scoles). Care must be taken to ensure that air is not trapped inside the tube end cover.

In addition to 275 W of heater power, the tube dissipates from 100 watts per ampere average anode current, rising to 300 W/A or greater at the highest rate of rise and fall of anode current.

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# PULSE MODULATOR SERVICE MAXIMUM AND MINIMUM RATINGS

	Min	Max
Anode		
Peak forward anode voltage		
(see note 3 and 4)	-	31 kV
Peak inverse anode voltage		see note 5
Peak forward anode current		
see (note 3)	-	5 kA
Average anode current	-	2 A
Rate of rise of anode current	. see i	notes 6 and 7
Pulse repetition rate		400 pps

### **Triggering**

For maximum life and minimum grid spike these thyratrons should be triggered with a pre-pulse on grid 1.

Min Max         Grid 2         Unloaded grid 2 drive pulse voltage (see note 8)       1000       2000       V         Grid 2 pulse duration       0.5       -       μs         Rate of rise of grid 2 pulse (see notes 7 and 9)       10       -       kV/μs         Grid 2 pulse delay (see note 10)       0.5       3.0       μs         Peak inverse grid 2 voltage       -       450       V         Loaded grid 2 bias voltage       -       100       -300       V         Impedance of grid 2 drive circuit (see note 11)       50       200       Ω         Impedance of grid 1 drive circuit (see note 11)       2.0       -       μs         Rate of rise of grid 1 pulse voltage       600       2000       V         Grid 1 pulse duration       2.0       -       μs         Rate of rise of grid 1 pulse       1.0       -       kV/μs         Peak inverse grid 1 voltage       -       450       V         Loaded grid 1 bias voltage       -       3.0       √         Peak grid 1 drive current (see note 13)       10.0       25.0       A         Cathode         Heater voltage       6.3 ± 0.3       V         Heating tim	should be triggered with a pre-pulse on	grid 1.
Unloaded grid 2 drive pulse voltage (see note 8)		Min Max
(see note 8)	Grid 2	
(see notes 7 and 9)	(see note 8)	
Peak inverse grid 2 voltage-450VLoaded grid 2 bias voltage100-300VImpedance of grid 2 drive circuit (see note 11)50200 $\Omega$ <b>Grid 1 - Pulsed</b> Unloaded grid 1 drive pulse voltage6002000VGrid 1 pulse duration2.0- $\mu$ sRate of rise of grid 1 pulse1.0-kV/ $\mu$ sPeak inverse grid 1 voltage-450VLoaded grid 1 bias voltage-see note 12Peak grid 1 drive current (see note 13)10.025.0A <b>Cathode</b> Heater voltage6.3 ± 0.3VHeating time10-min <b>Reservoir</b> Heater voltage6.3 ± 0.7V		10 - kV/μs
Loaded grid 2 bias voltage $-100$ $-300$ VImpedance of grid 2 drive circuit (see note 11) $50$ $200$ $\Omega$ Grid 1 - PulsedUnloaded grid 1 drive pulse voltage $600$ $2000$ VGrid 1 pulse duration $2.0$ $ \mu$ sRate of rise of grid 1 pulse $1.0$ $ kV/\mu$ sPeak inverse grid 1 voltage $ 450$ VLoaded grid 1 bias voltage $   -$ Peak grid 1 drive current (see note 13) $   -$ CathodeHeater voltage $     -$ ReservoirHeater voltage $     -$ Heater voltage $      -$	Grid 2 pulse delay (see note 10)	
Impedance of grid 2 drive circuit (see note 11)	Peak inverse grid 2 voltage	450 V
(see note 11)		-100 -300 V
Unloaded grid 1 drive pulse voltage $.600 2000 V$ Grid 1 pulse duration $ 2.0 - \mu s$ Rate of rise of grid 1 pulse $ 1.0 - kV/\mu s$ Peak inverse grid 1 voltage $ see note 12$ Peak grid 1 drive current (see note 13) $ 10.0 25.0 A$ Cathode Heater voltage $ 6.3 \pm 0.3 V$ Heating time $ 10 - min$ Reservoir		50 200 Ω
Unloaded grid 1 drive pulse voltage 600 2000 V Grid 1 pulse duration 2.0 - $\mu$ s Rate of rise of grid 1 pulse 1.0 - $kV/\mu$ s Peak inverse grid 1 voltage 5 - $kV/\mu$ s Peak grid 1 bias voltage 5 - $kV/\mu$ s 2 - $kV/\mu$ s Peak grid 1 drive current 6 - $kV/\mu$ s 2 - $kV$	Grid 1 - Pulsed	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		600 2000 V
Rate of rise of grid 1 pulse		
Peak inverse grid 1 voltage- $450$ VLoaded grid 1 bias voltage.see note 12Peak grid 1 drive current (see note 13). $10.0$ $25.0$ ACathodeHeater voltage $6.3 \pm 0.3$ VHeating time. $10$ -minReservoirHeater voltage $6.3 \pm 0.7$ - $0.3$ V		. 1.0 - kV/μs
Peak grid 1 drive current (see note 13)		· · · · · · · · · · · · · · · · · · ·
(see note 13)		see note 12
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(see note 13)	10.0 25.0 A
Heating time $10 - min$ Reservoir  Heater voltage $6.3 + 0.7 - 0.3$	Cathode	
<b>Reservoir</b> Heater voltage $6.3 + 0.7 - 0.3$ V	Heater voltage	. $6.3 \pm 0.3$ V
Heater voltage 6.3 + 0.7 V	Heating time	10 - min
	Reservoir	
	Heater voltage	$6.3 + 0.7 \\ - 0.3$
Heating time 10 - min	Heating time	10 - min
Environmental	Environmental	
Ambient temperature 0 +50 °C		. 0 +50 °C

### **CHARACTERISTICS**

	Min	Typical	Max	
Critical DC anode voltage for				
conduction	-	0.5	2.0	kV
Anode delay time	-	200	250	ns
Anode delay time drift				
(see note 14)	-	15	25	ns
Time jitter (see note 15)	-	1.0	5.0	ns
Recovery time (see note 16)	-	20	-	μs
Cathode heater current				
(at 6.3 V)	30	37.5	45	Α
Reservoir heater current				
(at 6.3 V)	6.0	7.0	8.0	Α

### **NOTES**

 It is recommended that the cathode heater and the reservoir heater are supplied from independent power supplies. The common connection for these two supplies is the yellow sleeved lead, not the cathode flange.

# N.B. The tube will suffer irreversible damage if the cathode flange is connected as the common point.

The cathode heater supply must be connected between the cathode flange and the cathode heater lead (yellow sleeve), the reservoir heater supply must be connected between the cathode heater lead (yellow sleeve) and the reservoir heater lead (red sleeve), see Fig. 1. In order to meet the jitter specification, it may be necessary in some circumstances that the cathode heater be supplied from a DC source.

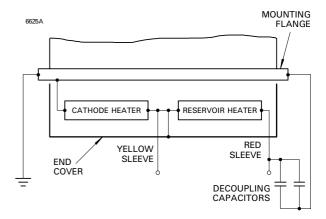


Fig. 1 CX1725W base connections

Care should be taken to ensure that excessive voltages are not applied to the reservoir heater circuit from the cathode heater supply because of high impedance cathode heater connections. For example, in the worst case, an open circuit heater lead will impress almost double voltage on the reservoir heater, especially on switch-on, when the cathode heater impedance is minimal. This situation can be avoided by ensuring that the two supplies are in antiphase. The reservoir heater circuit must be decoupled with suitable capacitors, for example, a 1  $\mu\text{F}$  capacitor in parallel with a low inductance 1000 pF capacitor.

CX1725W, page 2 © e2v technologies

The heater supply systems should be connected directly between the cathode flange and the heater leads. This avoids the possibility of injecting voltages into the cathode and reservoir heaters. At high rates of rise of anode current, the cathode potential may rise significantly at the beginning of the pulse, depending on the cathode lead inductance, which must be minimised at all times.

If a single transformer is used to supply both the cathode heater and the reservoir heater, then the reservoir heater lead (red sleeve) must be connected to the mounting flange.

- 2. The tube must be fitted using its mounting flange, with flexible connections to all other electrodes. The preferred orientation is with the tube axis vertical and anode uppermost; mounting the tube with its axis horizontal is permissible. It is **not** recommended that the tube is mounted with its axis vertical and cathode uppermost.
- 3. The CX1725W is structurally identical to the CX1725, which is rated for peak forward voltage of 70 kV max, peak forward current of 15 kA max. However, the internal deuterium gas pressure of the CX1725W is optimised at the factory for efficient operation at these conditions.
- The maximum permissible peak forward voltage for instantaneous starting is 31 kV and there must be no overshoot
- Due to the bidirectional switching capability of the tube, the presence of any reverse voltages following the forward current pulse will result in reverse current.
- 6. The ultimate value which can be attained depends to a large extent upon the external circuit. The rate of rise of current can be well in excess of 100 kA/ $\mu$ s.
- 7. This rate of rise refers to that part of the leading edge of the pulse between 10% and 90% of the pulse amplitude.
- 8. Measured with respect to cathode.
- A lower rate of rise may be used, but this may result in the anode delay time, delay time drift and jitter exceeding the limits quoted.
- 10. The last 0.25  $\mu s$  of the top of the grid 1 pulse must overlap the corresponding first 0.25  $\mu s$  of the top of the delayed grid 2 pulse.
- During both the drive pulse period and during recovery when the current flow is reversed.
- 12. DC negative bias voltages must not be applied to grid 1.

- 13. The optimum grid 1 pulse current is the maximum value which can be applied without causing the tube to switch before the grid 2 pulse is applied. This value is variable depending on gas pressure, maximum forward anode voltage, grid 2 negative bias voltage, peak current and repetition rate.
- 14. Measured between the second minute after the application of HT and 30 minutes later.
- 15. A time jitter of less than 1 ns can be obtained if the cathode heater voltage is supplied from a DC source and by applying a grid 2 pulse with a rate of rise of voltage (unloaded) in excess of 20 kV/ $\mu$ s.
- 16. The amount of time available for thyratron recovery must be maximised by circuit design, and reliable operation may necessitate the use of command charging techniques. The amount of time required for recovery is affected by gas pressure, peak current, pulse duration and load mismatch which keeps the thyratron in a conducting state.

### **HEALTH AND SAFETY HAZARDS**

e2v technologies hydrogen thyratrons are safe to handle and operate, provided that the relevant precautions stated herein are observed. e2v technologies does not accept responsibility for damage or injury resulting from the use of electronic devices it produces. Equipment manufacturers and users must ensure that adequate precautions are taken. Appropriate warning labels and notices must be provided on equipments incorporating e2v technologies devices and in operating manuals.



### High Voltage

Equipment must be designed so that personnel cannot come into contact with high voltage circuits. All high voltage circuits and terminals must be enclosed and fail-safe interlock switches must be fitted to disconnect the primary power supply and discharge all high voltage capacitors and other stored charges before allowing access. Interlock switches must not be bypassed to allow operation with access doors open.



### X-Ray Radiation

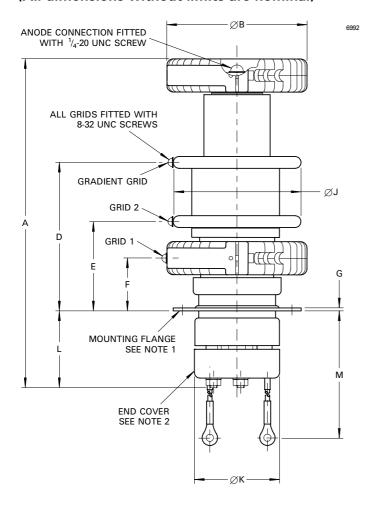
All high voltage devices produce X-rays during operation and may require shielding. The X-ray radiation from hydrogen thyratrons is usually reduced to a safe level by enclosing the equipment or shielding the thyratron with at least 1.6 mm ( $^{1}$ / $_{16}$  inch) thick steel panels.

Users and equipment manufacturers must check the radiation level under their maximum operating conditions.

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### **OUTLINE**

### (All dimensions without limits are nominal)



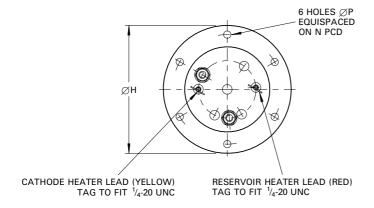
Ref	Millimetres	Inches
Α	288.0	11.338
В	122.0 max	4.803 max
D	131.0	5.157
Е	80.0	3.150
F	46.0	1.811
G	2.50	0.100
Н	111.13	4.375
J	111.13	4.375
K	75.0 max	2.953 max
L	70.0 max	2.756 max
M	381.0	15.000
Ν	95.25	3.750 max
Р	6.50	0.256

Inch dimensions have been derived from millimetres.

### **Outline Notes**

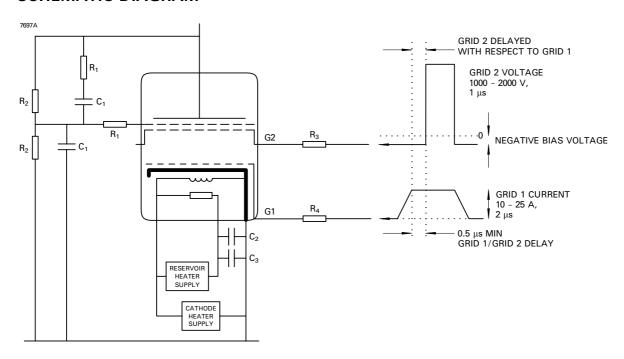
- 1. The mounting flange is the connection for the cathode and cathode heater return.
- 2. The end cover is at heater potential and must not be grounded.

### **Detail of Mounting Flange**



CX1725W, page 4 © e2v technologies

### **SCHEMATIC DIAGRAM**



### **Recommended Values**

- $R_1 = 470 \Omega 2.5 W vitreous enamelled wirewound resistors.$
- $R_2$  = 5 to 20 M $\Omega$  high voltage resistors with a power rating consistent with forward anode voltage.
- R<sub>3</sub> = Grid 2 series resistor. 12 W vitreous enamelled wirewound is recommended, of an impedance to match the grid 2 drive pulse circuit.
- R<sub>4</sub> = Grid 1 series resistor. 12 W vitreous enamelled wirewound is recommended, of a total impedance to match the grid 1 drive pulse circuit.
- $C_1$  = 500 pF capacitors with a voltage rating equal to the peak forward voltage ( $C_1$  is needed to share the anode voltage equally between the high voltage gaps on fast charging rates. When the charging time is greater than approx. 5 ms,  $C_1$  may be omitted).
- $C_2$ ,  $C_3$  reservoir protection capacitors with a voltage rating  $\geq 500 \text{ V}$ ;
  - $C_2 = 1000 \text{ pF low inductance (e.g. ceramic)},$
  - $C_3 = 1 \mu F$  (e.g. polycarbonate or polypropylene).

Components R<sub>3</sub>, R<sub>4</sub>, C<sub>2</sub> and C<sub>3</sub> should be mounted as close to the tube as possible.

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